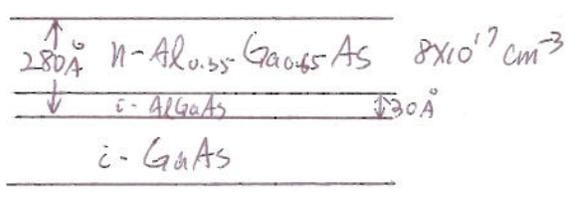


ECE 6453 HW# 6 Solution
(Selected)

6.2



$L_g = 0.25 \mu\text{m}$
 $W_g = 500 \mu\text{m}$
 $\phi_B = 1.0 \text{ eV}$

$V_{GS} = 0.3 \text{ V}, V_{DS} = 2 \text{ V}$

(a) $\phi_{00}' = \frac{1.6 \times 10^{-19} \times 8 \times 10^{17}}{2 \times 1.159 \times 10^{-12}} (250 \times 10^{-8})^2 = 0.345 \text{ (V)}$

$\frac{E_{f_0}}{q} = 0.0518 \text{ (V)}$ (P. 337 of Liu's)

$V_T = 1.0 + 0.0518 - 0.345 - 0.244 = \underline{0.463 \text{ (V)}}$

(b.) ~ (d) calculate α :

$V_{DSat} = V_{GS} - V_T = 0.3 - 0.463 = -0.163 < 0 \dots$

actually, $V_T = 0.463 \text{ (V)} > V_{GS} \Rightarrow$ The HFET is cut-off

$\Rightarrow \boxed{g_m = g_d = 0}$

$\Rightarrow \alpha = 0, C_{ox}' = \frac{1.159 \times 10^{-12}}{280 \times 10^{-8} + 68 \times 10^{-8}} = 3.33 \times 10^{-7} \text{ F/cm}^2$

$\therefore C_{gs} = WL C_{ox}' \cdot \frac{2}{3} = 4.1625 \times \frac{2}{3} = 2.78 \times 10^{-13} \text{ F}$

$C_{gg} = WL C_{ox}' \cdot \frac{2}{3} = 2.775 \times 10^{-13} \text{ F}$

$C_{gd} = WL C_{ox}' \cdot 0 = 0$

$C_{dg} = WL C_{ox}' \cdot \frac{4}{15} = 1.11 \times 10^{-13} \text{ F}$

$C_{dd} = WL C_{ox}' \cdot 0 = 0$

Common-source y-parameters:

$$[Y] = \begin{bmatrix} Y_{gg} & Y_{gd} \\ Y_{dg} & Y_{dd} \end{bmatrix} \quad \text{Assume quasi-static,}$$

$$Y_{gg} = j\omega C_{gg} = j\omega \times 2.775 \times 10^{-13}$$

$$Y_{gd} = -j\omega C_{gd} = 0$$

$$Y_{dg} = g_m - j\omega C_{dg} = -j\omega \times 1.11 \times 10^{-13}$$

$$Y_{dd} = g_d + j\omega C_{dd} = 0$$

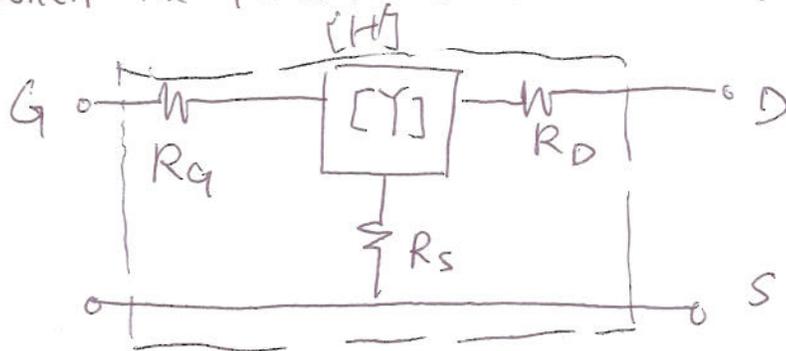
$$[Y] = \begin{bmatrix} j\omega \times 2.775 \times 10^{-13} & 0 \\ -j\omega \times 1.11 \times 10^{-13} & 0 \end{bmatrix} = j\omega \begin{bmatrix} 2.775 \times 10^{-13} & 0 \\ -1.11 \times 10^{-13} & 0 \end{bmatrix}$$

Note that the bias condition at $V_{gs} < V_T \Rightarrow$ The channel is not formed w/ $V_{gs} = 0.3V$. The only small-signal components left in the y-parameters are capacitive.

6.10

$$[Y] = \begin{bmatrix} j\omega C_{gg} & -j\omega C_{gd} \\ g_m - j\omega C_{dg} & g_d + j\omega C_{dd} \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} j4 \times 10^{-3} & -j3 \times 10^{-3} \\ 0.4 - j1 \times 10^{-3} & 0.1 + j9.5 \times 10^{-4} \end{bmatrix}$$

When the parasitic resistances ~~are~~ are included,



with the help of (6-232) & (6-233) & the conversion table ~~table~~ provided in the class, one may find the ~~the~~ h'_{21} of the new two-port network is:

$$h'_{21} = + \frac{-Z'_{21}}{Z'_{22}} = - \frac{R_S - y_{21}/\Delta}{R_D + R_S + y_{11}/\Delta}$$

$$= + \frac{y_{21} - R_S \Delta}{y_{11} + (R_S + R_D) \Delta}, \quad \Delta = y_{11} y_{22} - y_{12} y_{21}$$

Calculate $\Delta = j(4 \times 10^{-3}) \times [0.1 + j9.5 \times 10^{-4}] + [j3 \times 10^{-3} \times (0.4 - j1 \times 10^{-3})]$

$$\Rightarrow h'_{21} = \underline{-0.45 - j23.81} \neq$$

Note that, if you use the equation provided in eq. (6-234), you will never get this answer. (Because that equation is just an approximation form ~~equation~~ \rightarrow find the correction by yourself!!!)

$$U = \frac{|(y_{12} - y_{21})/\Delta y|^2}{4 \left\{ \operatorname{Re}(R_{st} R_G + y_{22}/\Delta y) \operatorname{Re}(R_{st} R_O + y_{11}/\Delta y) - \operatorname{Re}(R_S - y_{12}/\Delta y) \operatorname{Re}(R_S - y_{21}/\Delta y) \right\}}$$

$$U = 150.2$$

3.1 $\beta = \frac{I_C}{I_B} \approx \frac{I_C}{I_{Bp} + I_{B,bulk}}$

$$I_{B,bulk} = A_E \frac{q n_{iB}^2 W_B}{2 N_B \tau_n} \exp\left(\frac{qV_{BE}}{KT}\right)$$

$$I_{Bp} = A_E \frac{q D_{pE} n_{iE}^2}{W_E N_E} \exp\left(-\frac{\Delta E_V}{KT}\right) \exp\left(\frac{qV_{BE}}{KT}\right)$$

$$I_C \approx A_E \frac{q D_{nB} n_{iB}^2}{W_B N_B} \exp\left(\frac{qV_{BE}}{KT}\right)$$

From 1.7. estimate τ_n , D_{pE} , D_{nB} , n_{iE} , & n_{iB}

For example, $\tau_n \approx 2 \times 10^{-9}$ ns for $N_B = 5 \times 10^{18} \text{ cm}^{-3}$

$\tau_n = 10^{-11}$ ns for $N_B = 1 \times 10^{20} \text{ cm}^{-3}$

$$n_{iE} = n_{iAl_{0.35}Ga_{0.65}As} = 3.6 \times 10^2 \text{ cm}^{-3}$$

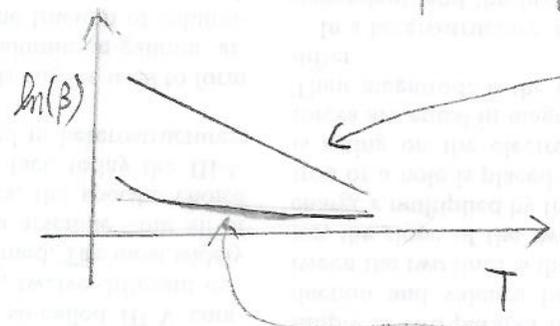
$$n_{iB} = n_{iGaAs} = 1.79 \times 10^6 \text{ cm}^{-3}$$

$$\beta = \frac{\frac{D_{nB} n_{iB}^2}{W_B N_B} \exp\left(\frac{qV_{BE}}{KT}\right)}{\frac{q n_{iB}^2 W_B}{2 N_B \tau_n} + \frac{D_{pE} n_{iE}^2}{W_E N_E} \exp\left(-\frac{\Delta E_V}{KT}\right)}$$

Note that the text book assume that $n_{iB} = n_{iE}$ which is not totally true -- You know why.

Assume that the temperature range is set s.t. D_n, D_p are constants.

(a) at $N_B = 5 \times 10^{18} \text{ cm}^{-3}$, $I_{B, \text{bulk}}$ is about 200X lower than that for $N_B = 10^{20} \text{ cm}^{-3}$. We will expect $\beta \propto \exp(\Delta E_V / kT)$,



(b) at $N_B = 10^{20} \text{ cm}^{-3}$, $I_{B, \text{bulk}} \approx I_{B, D}$

$$\beta = \frac{1}{\tau_B + \frac{D_{PE} n_{iE}^2 W_B N_B}{D_{nB} n_{iB}^2 W_E N_E} \exp\left(-\frac{\Delta E_V}{kT}\right)}$$

$$\tau_B = \frac{W_B^2}{2 \tau_n D_{nB}}$$